

eota@tzus.cz

190 00 Prague **Czech Republic** 





## **European Technical** Assessment

## ETA 14/0138 of 20/05/2018

<b>Technical Assessment Body issuing the ETA:</b> Technical and Test Institute for Construction Prague				
Trade name of the construction product	MO-H, MO-HW, MO-HS steel bonded anchor			
Product family to which the construction product belongs	Product area code: 33 Bonded injection type anchor for use in cracked and uncracked concrete			
Manufacturer	Index Técnicas Expansivas, S.L. P.I. La Portalada II C. Segador 13 26006 Logroño Spain			
Manufacturing plant	Index Plant 1			
This European Technical Assessment contains	19 pages including 15 Annexes which form an integral part of this assessment.			
This European Technical Assessment is issued in accordance with regulation (EU) No 305/2011, on the basis of	EAD 330499-00-0601			
This version replaces	ETA 14/0138 issued on 17/03/2016			

Translations of this European Technical Assessment in other languages shall fully correspond to the original issued document and should be identified as such.

Communication of this European Technical Assessment, including transmission by electronic means, shall be in full (excepted the confidential Annex(es) referred to above). However, partial reproduction may be made, with the written consent of the issuing Technical Assessment Body - Technical and Test Institute for Construction Prague. Any partial reproduction has to be identified as such.

#### 1. Technical description of the product

The MO-H, MO-HW (faster curing time) and MO-HS (extended processing time) with steel elements is bonded anchor (injection type).

Steel elements can be galvanized or stainless steel threaded rod or rebar.

Steel element is placed into a drilled hole filled with injection mortar. The steel element is anchored via the bond between metal part, injection mortar and concrete. The anchor is intended to be used with embedment depth from 8 diameters to 20 diameters.

The illustration and the description of the product are given in Annex A.

#### 2. Specification of the intended use in accordance with the applicable EAD

The performances given in Section 3 are only valid if the anchor is used in compliance with the specifications and conditions given in Annex B.

The provisions made in this European Technical Assessment are based on an assumed working life of the anchor of 50 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the products in relation to the expected economically reasonable working life of the works.

## 3. Performance of the product and references to the methods used for its assessment

#### 3.1 Mechanical resistance and stability (BWR 1)

Essential characteristic	Performance				
Static and quasi-static loading					
Resistance to steel failure (tension)	See Annex C1, C2				
Resistance to combined pull-out and concrete failure	See Annex C1, C2				
Resistance to concrete cone failure	See Annex C1, C2				
Edge distance to prevent splitting under load	See Annex C1, C2				
Robustness	See Annex C1, C2				
Maximum setting torque moment	See Annex B4				
Minimum edge distance and spacing	See Annex B4				
Resistance to steel failure (shear)	See Annex C3, C4				
Resistance to pry-out failure	See Annex C3, C4				
Resistance to concrete edge failure	See Annex C3, C4				
Displacements under short term and long term loading	See Annex C5, C6				
Durability of metal parts	See Annex A3				
Seismic performance C1					
Resistance to steel failure	See Annex C7				
Resistance to pull-out	See Annex C7				
Factor for annular gap	See Annex C7				

#### 3.2 Hygiene, health and environment (BWR 3)

No performance determined.

#### 3.3 General aspects relating to fitness for use

Durability and serviceability are only ensured if the specifications of intended use according to Annex B 1 are kept.

# 4. Assessment and verification of constancy of performance (AVCP) system applied with reference to its legal base

According to the Decision 96/582/EC of the European Commission<sup>1</sup> the system of assessment verification of constancy of performance (see Annex V to Regulation (EU) No 305/2011) given in the following table apply.

Product	Intended use	Level or class	System
	For fixing and/or supporting to concrete, structural elements (which contributes to the stability of the works) or heavy units	-	1

# 5. Technical details necessary for the implementation of the AVCP system, as provided in the applicable EAD

#### 5.1 Tasks of the manufacturer

The manufacturer may only use raw materials stated in the technical documentation of this European Technical Assessment.

The factory production control shall be in accordance with the control plan which is a part of the technical documentation of this European Technical Assessment. The control plan is laid down in the context of the factory production control system operated by the manufacturer and deposited at Technical and Test Institute for Construction Prague.<sup>2</sup> The results of factory production control shall be recorded and evaluated in accordance with the provisions of the control plan.

#### 5.2 Tasks of the notified bodies

The notified body shall retain the essential points of its actions referred to above and state the results obtained and conclusions drawn in a written report.

The notified certification body involved by the manufacturer shall issue a certificate of constancy of performance of the product stating the conformity with the provisions of this European Technical Assessment.

In cases where the provisions of the European Technical Assessment and its control plan are no longer fulfilled the notified body shall withdraw the certificate of constancy of performance and inform Technical and Test Institute for Construction Prague without delay.

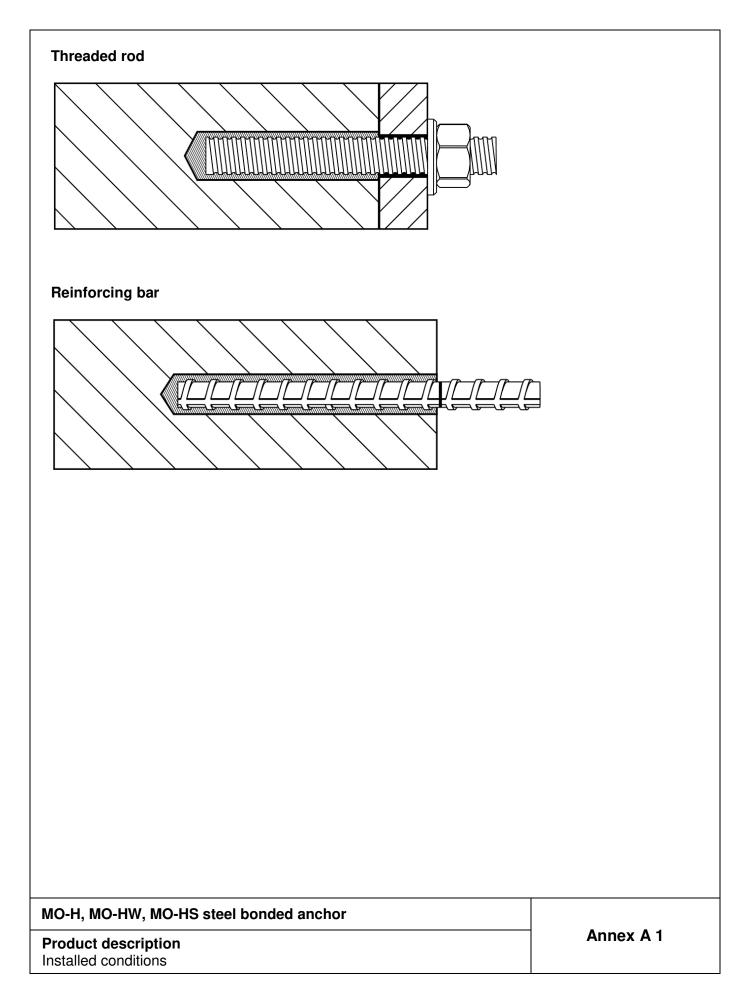
Issued in Prague on 20.05.2018

By

Ing. Mária Schaan Head of the Technical Assessment Body

<sup>&</sup>lt;sup>1</sup> Official Journal of the European Communities L 254 of 08.10.1996

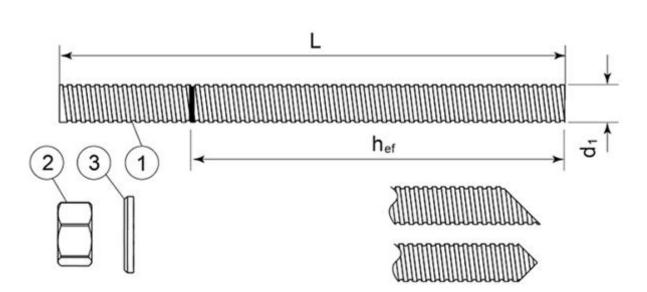
<sup>&</sup>lt;sup>2</sup> The control plan is a confidential part of the documentation of the European Technical Assessment, but not published together with the ETA and only handed over to the approved body involved in the procedure of AVCP.



Coaxial cartridge (CC) MO-H, MO-HW, MO-HS	150 ml 380 ml 400 ml 410 ml	
Side by side cartridge (SBS) MO-H, MO-HW, MO-HS	350 ml 825 ml	
<b>Two part foil in a single piston o</b> MO-H, MO-HW, MO-HS	component cartridge (FCC) 150 ml 170 ml 300 ml 550 ml 850 ml	
<b>Peeler cartridge (PLR)</b> MO-H, MO-HW, MO-HS	280 ml	
Marking of the mortar cartridges Identifying mark of the producer, T and processing time	s rade name, Charge code number, Storag	ge life, Curing
Mixing nozzle KW		
RC		
RM		
ТВ		
KR for use with 850		
MO-H, MO-HW, MO-HS steel bon	ded anchor	
Product description		Annex A 2

Injection system

#### Threaded rod M8, M10, M12, M16, M20, M24, M27, M30



Standard commercial threaded rod with marked embedment depth

Part	<b>,</b>	Material
Stee	I, zinc plated ≥ 5 μm acc. to EN IS0 I, Hot-dip galvanized ≥ 40 μm acc. I, zinc diffusion coating ≥ 15 μm a	to EN ISO 1461 and EN ISO 10684 or
1	Anchor rod	Steel, EN 10087 or EN 10263 Property class 4.6, 5.8, 8.8, 10.9* EN ISO 898-
2	Hexagon nut EN ISO 4032	According to threaded rod, EN 20898-2
3	Washer EN ISO 887, EN ISO 7089, EN ISO 7093 or EN ISO 7094	According to threaded rod
Stair	nless steel	
1	Anchor rod	Material: A2-70, A4-70, A4-80, EN ISO 3506
2	Hexagon nut EN ISO 4032	According to threaded rod
3	Washer EN ISO 887, EN ISO 7089, EN ISO 7093 or EN ISO 7094	According to threaded rod
High	corrosion resistant steel	
1	Anchor rod	Material: 1.4529, 1.4565, EN 10088-1
2	Hexagon nut EN ISO 4032	According to threaded rod
3	Washer EN ISO 887, EN ISO 7089, EN ISO 7093 or EN ISO 7094	According to threaded rod
*Galv	anized rod of high strength are sens	sitive to hydrogen induced brittle failure
יחי	MO-HW, MO-HS steel bonded ancl	bor
י-ח, ו		
	n de la Parte a	Annex A 3

### Product description

Threaded rod and materials

## Rebar Ø8, Ø10, Ø12, Ø16, Ø20, Ø25, Ø32

Standard commercial reinforcing bar with marked embedment depth

Product form	Bars and de	-coiled rods		
Class		В	С	
Characteristic yield strength fyk or fo	<sub>D,2k</sub> (MPa)	400 te	o 600	
Minimum value of $k = (f_t/f_y)_k$	≥ 1,08	≥ 1,15 < 1,35		
Characteristic strain at maximum for	orce ε <sub>uk</sub> (%)	≥ 5,0	≥ 7,5	
Bendability		Bend/Rebend test		
Maximum deviation from nominal	Nominal bar size (mm)			
mass (individual bar) (%)	≤ 8	±6,0		
	>8			
Bond: Minimum relative rib area,				
f <sub>R,min</sub>	0,040			
	> 12	0,056		

### MO-H, MO-HW, MO-HS steel bonded anchor

**Product description** Rebars and materials Annex A 4

#### Specifications of intended use

#### Anchorages subject to:

- Static and quasi-static load.
- Seismic actions category C1 (max w = 0,5 mm): threaded rod size M10, M12, M16, M20, M24

#### **Base materials**

- Uncracked concrete.
- Cracked and uncracked concrete for threaded rod size M10, M12, M16, M20, M24
- Reinforced or unreinforced normal weight concrete of strength class C20/25 at minimum and C50/60 at maximum according EN 206-1:2000-12.

#### Temperature range:

• -40°C to +80°C (max. short. term temperature +80°C and max. long term temperature +50°C)

#### Use conditions (Environmental conditions)

- (X1) Structures subject to dry internal conditions (zinc coated steel, stainless steel, high corrosion resistance steel).
- (X2) Structures subject to external atmospheric exposure (including industrial and marine environment) and to permanently damp internal condition, if no particular aggressive conditions exist (stainless steel A4, high corrosion resistant steel).
- (X3) Structures subject to external atmospheric exposure and to permanently damp internal condition, if other particular aggressive conditions exist (high corrosion resistant steel).

Note: Particular aggressive conditions are e.g. permanent, alternating immersion in seawater or the splash zone of seawater, chloride atmosphere of indoor swimming pools or atmosphere with extreme chemical pollution (e.g. in desulphurization plants or road tunnels where de-icing materials are used).

#### **Concrete conditions:**

- 11 installation in dry or wet (water saturated) concrete or flooded hole.
- I2 installation in water-filled (not sea water) and use in service in dry or wet concrete

#### Design:

- The anchorages are designed in accordance with the EN 1992-4 or EOTA Technical Report TR 055 under the responsibility of an engineer experienced in anchorages and concrete work.
- Verifiable calculation notes and drawings are prepared taking account of the loads to be anchored. The position of the anchor is indicated on the design drawings.
- Anchorages under seismic actions (cracked concrete) have to be designed in accordance with EN 1992-4.

#### Installation:

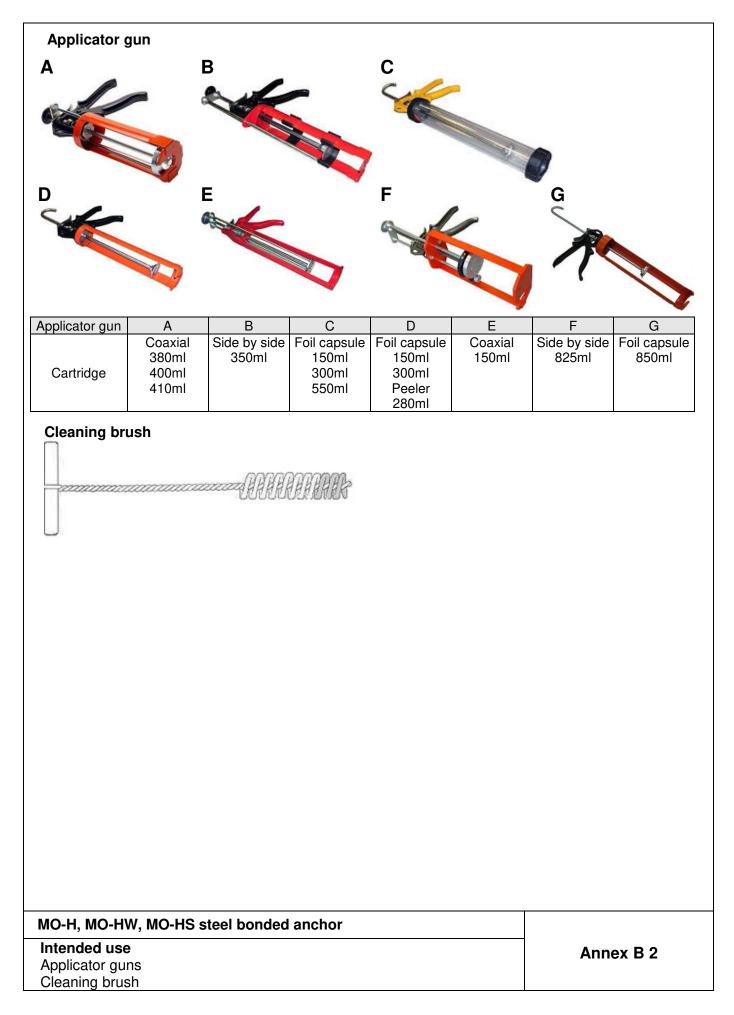
- Hole drilling by hammer drill mode.
- Anchor installation carried out by appropriately qualified personnel and under the supervision of the person responsible for technical matters of the site.

#### Installation direction:

• D3 – downward and horizontal and upwards (e.g. overhead) installation

#### MO-H, MO-HW, MO-HS steel bonded anchor

Intended use Specifications



#### Installation instructions

- 1. Drill the hole to the correct diameter and depth using a rotary percussion drilling machine.
- 2. Thoroughly clean the hole in the following sequence using the brush with the required extensions and a blow pump:

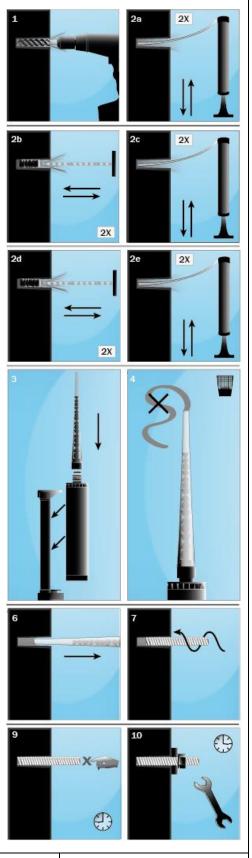
Blow Clean x2. Brush Clean x2. Blow Clean x2. Brush Clean x2. Blow Clean x2.

Remove standing water from the hole prior to cleaning to achieve maximum performance.

- 3. Select the appropriate static mixer nozzle for the installation, open the cartridge/cut foil pack and screw nozzle onto the mouth of the cartridge. Insert the cartridge into a good quality applicator (gun).
- 4. Extrude the first part of the cartridge to waste until an even colour has been achieved without streaking in the resin.
- 5. If necessary, cut the extension tube to the depth of the hole and push onto the end of the mixer nozzle, and fit the correct resin stopper to the other end.
- 6. Insert the mixer nozzle (or the extension tube with resin stopper when necessary) to the bottom of the hole. Begin to extrude the resin and slowly withdraw the mixer nozzle from the hole ensuring that there are no air voids as the mixer nozzle is withdrawn. Fill the hole to approximately ½ to ¾ full and withdraw the nozzle completely.
- 7. Insert the clean threaded bar, free from oil or other release agents, to the bottom of the hole using a back and forth twisting motion ensuring all the threads are thoroughly coated. Adjust to the correct position within the stated working time.
- Excess resin will be expelled from the hole evenly around the steel element showing that the hole is full.
   This excess resin should be removed from around the mouth of the hole before it sets.
- Leave the anchor to cure.
   Do not disturb the anchor until the appropriate loading time has elapsed depending on the substrate conditions and ambient temperature.
- 10. Attach the fixture and tighten the nut to the recommended torque. **Do not overtighten**.



#### Intended use Installation procedure



Annex B 3

Table B1: Installation parameters of threaded rod										
Size			M8	M10	M12	M16	M20	M24	M27	M30
Nominal drill hole diameter	$\operatorname{Ød}_0$	[mm]	10	12	14	18	22	26	30	35
Diameter of cleaning brush	db	[mm]	14	14	20	20	29	29	40	40
Torque moment	max T <sub>fix</sub>	[Nm]	10	20	40	80	150	200	240	275
Depth of drill hole for hef,min	$h_0 = h_{ef}$	[mm]	64	80	96	128	160	192	216	240
Depth of drill hole for hef,max	$h_0 = h_{ef}$	[mm]	160	200	240	320	400	480	540	600
Minimum edge distance	C <sub>min</sub>	[mm]	35	40	50	65	80	96	110	120
Minimum spacing	Smin	[mm]	35	40	50	65	80	96	110	120
Minimum thickness of member	$h_{\text{min}}$	[mm]	h <sub>ef</sub> +	30 mn	n ≥ 100	) mm		h <sub>ef</sub> +	- 2d <sub>0</sub>	

#### Table B2: Installation parameters of rebar

Size			Ø8	Ø10	Ø12	Ø16	Ø20	Ø25	Ø32
Nominal drill hole diameter	$\operatorname{Ød}_0$	[mm]	12	14	16	20	25	32	40
Diameter of cleaning brush	db	[mm]	14	14	19	22	29	40	42
Depth of drill hole for hef,min	$h_0 = h_{ef}$	[mm]	64	80	96	128	160	200	256
Depth of drill hole for hef,max	$h_0 = h_{ef}$	[mm]	160	200	240	320	400	500	640
Minimum edge distance	Cmin	[mm]	35	40	50	65	80	100	130
Minimum spacing	Smin	[mm]	35	40	50	65	80	100	130
Minimum thickness of member	h <sub>min</sub>	[mm]	h <sub>ef</sub> -	+ 30 mn	า ≥ 100	mm		h <sub>ef</sub> + 2d	ט

#### Table B3: Cleaning

All diameters
- 2 x blowing
- 2 x brushing
- 2 x blowing
- 2 x brushing
- 2 x blowing

#### Table B4: Minimum curing time

MO-H		
Application temperature	Processing time	Load time
+5 to +10°C	10 mins	145 mins
+10 to +15°C	8 mins	85 mins
+15 to +20°C	6 mins	75 mins
+20 to +25°C	5 mins	50 mins
+25 to +30°C	4 mins	40 mins

Processing time refers to the highest temperature in the range. Load time refers to the lowest temperature in the range. Cartridge must be conditioned to a minimum  $+5^{\circ}$ C.

MO-HW		
Application temperature	Processing time	Load time
0 to +5°C	10 mins	75 mins
+5 to +20°C	5 mins	50 mins
+20°C	100 second	20 mins

Processing time refers to the highest temperature in the range. Load time refers to the lowest temperature in the range. Cartridge must be conditioned to a minimum 0°C.

MO-HS		
Application temperature	Processing time	Load time
+15 to +20°C	15 mins	5 hours

+15 to +20°C	15 mins	5 hours
+20 to +25°C	10 mins	145 mins
+25 to +30°C	7.5 mins	85 mins
+30 to +35°C	5 mins	50 mins
+35 to +40°C	3.5 mins	40 mins

Processing time refers to the highest temperature in the range. Load time refers to the lowest temperature in the range. Cartridge must be conditioned to a minimum  $+15^{\circ}$ C.

#### MO-H, MO-HW, MO-HS steel bonded anchor

## Installation parameters Curing time

Annex B 4

Steel failure – Characteristic	resistance									
Size			M8	M10	M12	M16	M20	M24	M27	M30
Steel grade <b>4.6</b>	N <sub>Rk,s</sub>	[kN]	15	23	34	63	98	141	184	224
Partial safety factor	γMs	[-]				2,	00			
Steel grade <b>5.8</b>	N <sub>Rk,s</sub>	[kN]	18	29	42	79	123	177	230	281
Partial safety factor	γMs	[-]				1,	50			
Steel grade <b>8.8</b>	N <sub>Rk,s</sub>	[kN]	29	46	67	126	196	282	367	449
Partial safety factor	γMs	[-]			•	1,	50		•	
Steel grade 10.9	N <sub>Rk,s</sub>	[kN]	37	58	84	157	245	353	459	561
Partial safety factor	γMs	[-]			•	1,	33		•	
Stainless steel grade A2-70, A4-7		[kN]	26	41	59	110	172	247	321	393
Partial safety factor	γMs	[-]					87	•		
Stainless steel grade A4-80	N <sub>Rk,s</sub>	[kN]	29	46	67	126	196	282	367	449
Partial safety factor	γMs	[-]					60			
Stainless steel grade 1.4529	N <sub>Rk,s</sub>	[kN]	26	41	59	110	172	247	321	393
Partial safety factor	γMs	[-]					50			
Stainless steel grade <b>1.4565</b>	N <sub>Rk,s</sub>	[kN]	26	41	59	110	172	247	321	393
Partial safety factor	γMs	[-]					87			
•										
Combined pullout and concr	ete cone failu	ire in ur								
Size				M8   N	110 M	12 M	16 M2	20 M24	4 M27	7 M30
Characteristic bond resistan	ce in uncrack	ed con	crete							
Dry and wet concrete	$ au_{Rk,ucr}$	[N/mm	1 <sup>2</sup> ]	10 9	9,5 9	,5 9	) 8,	5 8	6,5	5,5
Installation safety factor	$\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[-]				1,2				1,4
Flooded hole	τ <sub>Rk,ucr</sub>		<sup>2</sup> ] {	8,5 7	7,5	7 7	7 6,	5 5,5		
Installation safety factor	$\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[-]		-,	,-		1,4	,-		
Factor for concrete C50/60	Ψc	[-]					1			
Combined pullout and concr	ete cone failu	ire in cr	acke	d con	crete (	C20/25				
Size				M10	M	10	M16	M2	<u>م</u>	M24
Characteristic bond resistan					IVI	12			U	
onaraoichisile pullu i CSISIdii	ce in cracked	concre	ete	mite	IVI	12	IN TO	IVIZ	U	1012-1
Dry and wet concrete	$ au_{Rk,cr}$			4,5	4,		4,5	4		4
Dry and wet concrete	$\tau_{Rk,cr}$ $\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2	4		4
Dry and wet concrete Installation safety factor Flooded hole	$ au_{Rk,cr}$ $\gamma_2^{(1)} = \gamma_{inst}^{(2)}$ $ au_{Rk,cr}$	[N/mm [-] [N/mm	1 <sup>2</sup> ]			5	4,5 1,2 4,5			
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor	$\begin{array}{c} & \tau_{\text{Rk,cr}} \\ & \gamma_2{}^{(1)} = \gamma_{\text{inst}}{}^{(2)} \\ & \tau_{\text{Rk,cr}} \\ & \gamma_2{}^{(1)} = \gamma_{\text{inst}}{}^{(2)} \end{array}$	[N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor	$\frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)} = \gamma_{\text{inst}}^{2}} \frac{\tau_{\text{Rk,cr}}}{\tau_{\text{Rk,cr}}}$ $\frac{\gamma_2^{1)} = \gamma_{\text{inst}}^{2}}{230/37}$	[N/mm [-] [N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete	$\frac{\frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)}=\gamma_{\text{inst}}^{2)}}{\tau_{\text{Rk,cr}}}}{\frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)}=\gamma_{\text{inst}}^{2)}}}$	[N/mm [-] [N/mm	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete	$\frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)} = \gamma_{\text{inst}}^{2}} \frac{\tau_{\text{Rk,cr}}}{\tau_{\text{Rk,cr}}}$ $\frac{\gamma_2^{1)} = \gamma_{\text{inst}}^{2}}{230/37}$	[N/mm [-] [N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete	$\frac{\frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)}=\gamma_{\text{inst}}^{2)}}{\tau_{\text{Rk,cr}}}}{\frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)}=\gamma_{\text{inst}}^{2)}}}$	[N/mm [-] [N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Concrete cone failure	$\begin{array}{c} \tau_{\text{Rk,cr}} \\ \gamma_2{}^{1)} = \gamma_{\text{inst}}{}^{2)} \\ \hline \tau_{\text{Rk,cr}} \\ \gamma_2{}^{1)} = \gamma_{\text{inst}}{}^{2)} \\ \tau_2{}^{30/37} \\ \tau_2{}^{30/37} \\ \tau_2{}^{40/50} \\ \tau_c \\ \tau$	[N/mm [-] [N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Concrete cone failure Factor for concrete cone failure	$\frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)} = \gamma_{\text{inst}}^{2)} \tau_{\text{Rk,cr}}} \frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)} = \gamma_{\text{inst}}^{2)}} \frac{\tau_{\text{Rk,cr}}}{\gamma_2^{10} = \gamma_{\text{inst}}^{2}} \frac{\gamma_2^{10}}{\gamma_2^{10}} \gamma_2$	[N/mm [-] [N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Concrete cone failure Factor for concrete cone failure for uncracked concrete	$\frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)} = \gamma_{\text{inst}}^{2)} \tau_{\text{Rk,cr}}} \frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)} = \gamma_{\text{inst}}^{2)}} \frac{\tau_{\text{Rk,cr}}}{\gamma_2^{10} = \gamma_{\text{inst}}^{2}} \frac{\gamma_2^{10}}{\gamma_2^{10}} \gamma_2$	[N/mm [-] [N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Concrete cone failure Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure	$\begin{array}{c} & TRk,cr \\ & \gamma 2^{1)} = \gamma inst^{2)} \\ & TRk,cr \\ & \gamma 2^{1)} = \gamma inst^{2)} \\ \hline & 0.0037 \\ $	[N/mm [-] [N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Concrete cone failure Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete	$\begin{array}{c} & {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ \hline \\ $	[N/mm [-] [N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Concrete cone failure Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Edge distance	$\begin{array}{c} & {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ \hline \\ $	[N/mm [-] [N/mm [-] [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5hef			4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Concrete cone failure Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete	$\begin{array}{c} & {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ \hline \\ $	[N/mm [-] [N/mm [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5hef	4		4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor	$\begin{array}{c} & {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ \hline \\ $	[N/mm [-] [N/mm [-] [-]	1 <sup>2</sup> ]	4,5	4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5hef			4
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Concrete cone failure Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure	$\begin{array}{c} & {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ {}^{\text{TRk,cr}} \\ \gamma_2{}^{1)} = \gamma_{inst}{}^{2)} \\ \hline \\ $	[N/mm [-] [N/mm [-] [-]		4,5 4,5 see Co	4, 4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> tt and c	4	cone fa	4 4 ailure
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size	$\begin{array}{c} & {}^{\text{TRk,cr}} \\ \gamma 2^{1)} = \gamma inst^{2)} \\ & {}^{\text{TRk,cr}} \\ \gamma 2^{1)} = \gamma inst^{2)} \\ \hline \\ $	[N/mm [-] [N/mm [-] [-]		4,5 4,5 see Co	4, 4,	5	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5hef it and c		cone fa	4 4 ailure
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Factor for concrete cone failure for cracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size Edge distance	$\frac{\tau_{Rk,cr}}{\gamma_2^{1)}=\gamma_{inst}^{2)}} \frac{\tau_{Rk,cr}}{\tau_{Rk,cr}}$ $\frac{\gamma_2^{1)}=\gamma_{inst}^{2)}}{230/37}$ $240/50  \psi_c$ $250/60$ $\frac{k_1^{11}}{k_{ucr,N}^{2)}}$ $\frac{k_1^{11}}{k_{cr,N}^{2}}$ $\frac{c_{cr,N}}{\gamma_2^{1)}=\gamma_{inst}^{2}}$	[N/mm [-] [N/mm [-] [-] [-]		4,5 4,5 see Co	4, 4,	5 5 5 4 6 pullou	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> it and c 16 M2 1,5h <sub>ef</sub>	4	cone fa	4 4 ailure
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size Edge distance Spacing	$\begin{array}{c} & {}^{\text{TRk,cr}} \\ \gamma 2^{1)} = \gamma inst^{2)} \\ & {}^{\text{TRk,cr}} \\ \gamma 2^{1)} = \gamma inst^{2)} \\ \hline \end{array} \\ \begin{array}{c} \hline \end{array} \\ \end{array} \\ \begin{array}{c} \hline \end{array} \\ \begin{array}{c} \hline \end{array} \\ \end{array} \\ \begin{array}{c} \hline \end{array} \\ \begin{array}{c} \hline \end{array} \\ \end{array} \\ \begin{array}{c} \hline \end{array} \\ \begin{array}{c} \hline \end{array} \\ \end{array} \\ \begin{array}{c} \hline \end{array} \\ \end{array} \\ \begin{array}{c} \hline \end{array} \\ \begin{array}{c} \hline \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \hline \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \hline \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \end{array} \\ \begin{array}{c} \hline \end{array} \\ \end{array}$	[N/mm [-] [N/mm [-] [-] [-]		4,5 4,5 see Co	4, 4,	5 5 5 4 d pullou 12 M	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> tt and c 1,5h <sub>ef</sub> 3,0h <sub>ef</sub>	4 4 0 4	cone fa	4 4 ailure 7   M30
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size Edge distance Spacing Installation safety factor	$\begin{array}{c} & {}^{\text{TRk,cr}} \\ & \gamma_2{}^{1)} {=} \gamma_{\text{inst}}{}^{2)} \\ & {}^{\text{TRk,cr}} \\ & \gamma_2{}^{1)} {=} \gamma_{\text{inst}}{}^{2)} \\ \hline & 230/37 \\ \hline & 240/50  \Psi_c \\ \hline & C50/60 \\ \hline \\ \hline & & k_{11} \\ \hline & k_{\text{ucr,N}}{}^{2)} \\ \hline & & k_{11} \\ \hline & k_{\text{ucr,N}}{}^{2)} \\ \hline & & k_{11} \\ \hline & k_{\text{cr,N}}{}^{2} \\ \hline & & c_{\text{cr,N}} \\ \hline & & \gamma_2{}^{1)} {=} \gamma_{\text{inst}}{}^{2} \\ \hline & & c_{\text{cr,sp}} \\ \hline & & s_{\text{cr,sp}} \\ \hline & & \gamma_2{}^{1)} {=} \gamma_{\text{inst}}{}^{2} \end{array}$	[N/mm [-] [N/mm [-] [-] [-]		4,5 4,5 see Co	4, 4,	5 5 5 4 d pullou 12 M	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> tt and c 1,5h <sub>ef</sub> 3,0h <sub>ef</sub>	4	cone fa	4 4 ailure 7   M30
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size Edge distance Spacing	$\begin{array}{c} & {}^{\text{TRk,cr}} \\ & \gamma_2{}^{1)} {=} \gamma_{\text{inst}}{}^{2)} \\ & {}^{\text{TRk,cr}} \\ & \gamma_2{}^{1)} {=} \gamma_{\text{inst}}{}^{2)} \\ \hline & 230/37 \\ \hline & 240/50  \Psi_c \\ \hline & C50/60 \\ \hline \\ \hline & & k_{11} \\ \hline & k_{\text{ucr,N}}{}^{2)} \\ \hline & & k_{11} \\ \hline & k_{\text{ucr,N}}{}^{2)} \\ \hline & & k_{11} \\ \hline & k_{\text{cr,N}}{}^{2} \\ \hline & & c_{\text{cr,N}} \\ \hline & & \gamma_2{}^{1)} {=} \gamma_{\text{inst}}{}^{2} \\ \hline & & c_{\text{cr,sp}} \\ \hline & & s_{\text{cr,sp}} \\ \hline & & \gamma_2{}^{1)} {=} \gamma_{\text{inst}}{}^{2} \end{array}$	[N/mm [-] [N/mm [-] [-] [-]		4,5 4,5 see Co	4, 4,	5 5 5 4 d pullou 12 M	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> tt and c 1,5h <sub>ef</sub> 3,0h <sub>ef</sub>	4 4 0 4	cone fa	4 4 ailure 7   M30
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size Edge distance Spacing Installation safety factor	$\frac{\tau_{\text{Rk,cr}}}{\gamma_2^{1)}=\gamma_{\text{inst}}^{2)}}$ $\frac{\tau_{\text{Rk,cr}}}{\gamma_{\text{Rk,cr}}}$ $\frac{\gamma_2^{1)}=\gamma_{\text{inst}}^{2)}}{\gamma_{\text{Cl}}}$ $\frac{\gamma_2^{1)}=\gamma_{\text{inst}}^{2}}{\gamma_{\text{Cl}}}$ $\frac{\gamma_2^{1)}=\gamma_{\text{inst}}^{2}}{\gamma_2^{1)}=\gamma_{\text{inst}}^{2}}$ $\frac{c_{\text{cr,N}}}{\gamma_2^{1)}=\gamma_{\text{inst}}^{2}}$ $\frac{c_{\text{cr,sp}}}{\gamma_2^{1)}=\gamma_{\text{inst}}^{2}}$ $c_{\text{chrical Report}}$	[N/mm [-] [N/mm [-] [-] [-]		4,5 4,5 see Co	4, 4,	5 5 5 4 d pullou 12 M	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> tt and c 1,5h <sub>ef</sub> 3,0h <sub>ef</sub>	4 4 0 4	cone fa	4 4 ailure 7   M30
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size Edge distance Spacing Installation safety factor <sup>1)</sup> Design according EOTA Tec <sup>2)</sup> Design according EN 1992-4	$\frac{\tau_{Rk,cr}}{\gamma_2^{1)}=\gamma_{inst}^{2)}} \frac{\tau_{Rk,cr}}{\tau_{Rk,cr}}$ $\frac{\gamma_2^{1)}=\gamma_{inst}^{2)}}{\gamma_2^{1)}=\gamma_{inst}^{2)}}$ $\frac{\zeta_{230/37}}{\zeta_{240/50}} \psi_c$ $\frac{\zeta_{250/60}}{\psi_c}$ $\frac{k_1^{11}}{k_{ucr,N^{2}}} \frac{k_1^{11}}{k_{ucr,N^{2}}} \frac{k_1^{11}}{k_{cr,N^{2}}} \frac{c_{cr,N}}{c_{cr,N}}}{\zeta_{cr,N}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2)}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2)}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$	[N/mm [-] [N/mm [-] [-] [-] [mm] [-] TR 055		4,5 4,5 see Co	4, 4,	5 5 5 4 d pullou 12 M	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> tt and c 1,5h <sub>ef</sub> 3,0h <sub>ef</sub>	4 4 0 4	cone fa	4 4 ailure 7   M30
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size Edge distance Spacing Installation safety factor 1) Design according EOTA Teo 2) Design according EN 1992-4 O-H, MO-HW, MO-HS stee	$\frac{\tau_{Rk,cr}}{\gamma_2^{1)}=\gamma_{inst}^{2)}} \frac{\tau_{Rk,cr}}{\tau_{Rk,cr}}$ $\frac{\gamma_2^{1)}=\gamma_{inst}^{2)}}{\gamma_2^{1)}=\gamma_{inst}^{2)}}$ $\frac{\zeta_{230/37}}{\zeta_{240/50}} \psi_c$ $\frac{\zeta_{250/60}}{\psi_c}$ $\frac{k_1^{11}}{k_{ucr,N^{2}}} \frac{k_1^{11}}{k_{ucr,N^{2}}} \frac{k_1^{11}}{k_{cr,N^{2}}} \frac{c_{cr,N}}{c_{cr,N}}}{\zeta_{cr,N}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2)}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2)}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$	[N/mm [-] [N/mm [-] [-] [-] [mm] [-] TR 055		4,5 4,5 see Co	4, 4,	5 5 5 4 d pullou 12 M	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> tt and c 1,5h <sub>ef</sub> 3,0h <sub>ef</sub>	4 4 0 4	cone fa	4 4 ailure 7   M30
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size Edge distance Spacing Installation safety factor <sup>1)</sup> Design according EOTA Tec <sup>2)</sup> Design according EN 1992-4	$\frac{\tau_{Rk,cr}}{\gamma_2^{1)}=\gamma_{inst}^{2)}} \frac{\tau_{Rk,cr}}{\tau_{Rk,cr}}$ $\frac{\gamma_2^{1)}=\gamma_{inst}^{2)}}{\gamma_2^{1)}=\gamma_{inst}^{2)}}$ $\frac{\zeta_{230/37}}{\zeta_{240/50}} \psi_c$ $\frac{\zeta_{250/60}}{\psi_c}$ $\frac{k_1^{11}}{k_{ucr,N^{2}}} \frac{k_1^{11}}{k_{ucr,N^{2}}} \frac{k_1^{11}}{k_{cr,N^{2}}} \frac{c_{cr,N}}{c_{cr,N}}}{\zeta_{cr,N}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2)}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2)}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$ $\frac{\zeta_{cr,sp}}{\gamma_2^{11}=\gamma_{inst}^{2}}$	[N/mm [-] [N/mm [-] [-] [-] [mm] [-] TR 055		4,5 4,5 see Co	4, 4,	5 5 5 4 d pullou 12 M	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> tt and c 1,5h <sub>ef</sub> 3,0h <sub>ef</sub>	4 4 0 4	cone fa	4 4 ailure 7 M30 ailure
Dry and wet concrete Installation safety factor Flooded hole Installation safety factor Factor for cracked concrete Factor for concrete cone failure for uncracked concrete Factor for concrete cone failure for cracked concrete Factor for concrete cone failure for cracked concrete Edge distance Installation safety factor Splitting failure Size Edge distance Spacing Installation safety factor 1) Design according EOTA Teo 2) Design according EN 1992-4 O-H, MO-HW, MO-HS stee	$\frac{\text{TRk,cr}}{\gamma 2^{1)} = \gamma \text{inst}^{2)}}$ $\frac{\text{TRk,cr}}{\gamma 2^{1)} = \gamma \text{inst}^{2)}}$ $\frac{\text{TRk,cr}}{\gamma 2^{1)} = \gamma \text{inst}^{2)}}$ $\frac{\text{C30/37}}{\text{C40/50}}$ $\frac{\text{C40/50}}{\text{C50/60}} \text{ $\psi_c$}$ $\frac{\text{C50/60}}{\text{C50/60}}$ $\frac{\text{C}_{cr,N^2}}{\text{C}_{cr,N^2}}$ $\frac{\text{C}_{cr,N^2}}{\text{C}_{cr,N}}$ $\frac{\gamma 2^{1)} = \gamma \text{inst}^{2)}}{\text{C}_{cr,Sp}}$ $\frac{\text{C}_{cr,Sp}}{\gamma 2^{1)} = \gamma \text{inst}^{2)}}$ $\frac{\text{Chnical Report}}{\text{C}_{cr,Sp}}$ $\frac{\text{Constant Report}}{\text{C}_{cr,Sp}}$	[N/mm [-] [N/mm [-] [-] [-] [mm] [-] TR 055		4,5 4,5 see Co	4, 4,	5 5 5 4 d pullou 12 M	4,5 1,2 4,5 1,4 1,12 1,23 1,30 10,1 11 7,2 7,7 1,5h <sub>ef</sub> tt and c 1,5h <sub>ef</sub> 3,0h <sub>ef</sub>	4 4 0 4	cone fa	4 4 ailure 7 M30 ailure

Page 13 of 19 ETA 14/0138 issued on 20/05/2018 and replacing ETA 14/0138 issued on 17/03/2016

# Table C2: Design method EN 1992-4 Characteristic values of resistance to tension load of rebar

Steel failure – Characteristic resistance											
Size			Ø8	Ø10	Ø12	Ø16	Ø20	Ø25	Ø32		
Rebar BSt 500 S	N <sub>Rk,s</sub>	[kN]	28	43	62	111	173	270	442		
Partial safety factor	γMs	[-]				1,4					

Combined pullout and concret	e cone failu	ire in unci	acked	concre	te C20	/25			
Size			Ø8	Ø10	Ø12	Ø16	Ø20	Ø25	Ø32
Characteristic bond resistance	e in uncrack	ed concre	ete						
Dry and wet concrete	τRk,ucr	[N/mm <sup>2</sup> ]	11	9,5	9,5	9	8,5	8,5	5,5
Installation safety factor	$\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[-]				1,2			
Flooded hole	τRk,ucr	[N/mm <sup>2</sup> ]	11	9,5	9,5	9	8,5	8,5	5,5
Installation safety factor	$\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[-]				1,4			
Factor for concrete C50/60	Ψc	[-]				1			

$k_1^{1)}$	[-]	10,1
k <sub>ucr,N</sub> 2)		11
Ccr,N	[mm]	1,5h <sub>ef</sub>
$\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[-]	see Combined pullout and concrete cone failure
	k <sub>ucr,N</sub> <sup>2)</sup> Ccr,N	k <sub>ucr,N</sub> <sup>2)</sup> C <sub>cr,N</sub> [mm]

Splitting failure									
Size			Ø8	Ø10	Ø12	Ø16	Ø20	Ø25	Ø32
Edge distance	C <sub>cr,sp</sub>	[mm]	1,5h <sub>ef</sub>						
Spacing	Scr,sp	[mm]	3,0h <sub>ef</sub>						
Installation safety factor	$\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[-]	see (	Combine	ed pullo	ut and c	oncrete	cone fa	ilure

<sup>1)</sup> Design according EOTA Technical Report TR 055

<sup>2)</sup> Design according EN 1992-4:2016

#### MO-H, MO-HW, MO-HS steel bonded anchor

#### **Performances** Design according to EN 1992-4 Characteristic resistance for tension loads - rebar

Steel failure without lever arm							-			
Size			M8	M10	M12	M16	M20	M24	M27	M30
Steel grade <b>4.6</b>	V <sub>Rk,s</sub>	[kN]	7	12	17	31	49	71	92	112
Partial safety factor	γMs	[-]				1,	67			
Steel grade <b>5.8</b>	$V_{Rk,s}$	[kN]	9	15	21	39	61	88	115	140
Partial safety factor	γMs	[-]				1,	25			
Steel grade 8.8	V <sub>Rk,s</sub>	[kN]	15	23	34	63	98	141	184	224
Partial safety factor	γMs	[-]				1,	25			
Steel grade 10.9	$V_{Rk,s}$	[kN]	18	29	42	79	123	177	230	281
Partial safety factor	γMs	[-]				1	,5			
Stainless steel grade A2-70, A4-70	$V_{Rk,s}$	[kN]	13	20	30	55	86	124	161	196
Partial safety factor	γMs	[-]				1,	56			
Stainless steel grade A4-80	$V_{Rk,s}$	[kN]	15	23	34	63	98	141	184	224
Partial safety factor	γMs	[-]				1,	33			
Stainless steel grade 1.4529	$V_{Rk,s}$	[kN]	13	20	30	55	86	124	161	196
Partial safety factor	γMs	[-]				1,	25			
Stainless steel grade 1.4565	$V_{Rk,s}$	[kN]	13	20	30	55	86	124	161	196
Partial safety factor	γMs					1,	56			
Characteristic resistance of group of fa	asteners	-	_							
Ductility factor $k_7 = 1,0$ for steel with ru	pture elo	ngation	$A_5 > 8$	3%						
Steel failure with lever arm										
Size			M8	M10	M12	M16	M20	M24	M27	M30
	M0	[N] m]	15	30	52	133		449		900
Steel grade <b>4.6</b> Partial safety factor	M <sup>o</sup> Rk,s		15	30	52		260 67	449	666	900
Steel grade <b>5.8</b>	γMs Mo-	[-] [N.m]	19	37	66	166	325	561	832	1125
Partial safety factor		[-]	19	37	00		25	501	032	1120
Steel grade 8.8	γMs M <sup>o</sup> Rk,s		30	60	105	266	519	898	1332	1700
Partial safety factor	IVI <sup>-</sup> Rk,s γMs	[13.111] [-]	30	00	105		25	090	1332	1795
Steel grade 10.9		[N.m]	37	75	131	333	649	1123	1664	2240
Partial safety factor			37	75	131		50	1123	1004	2243
Stainless steel grade A2-70, A4-70	γMs M <sup>o</sup> Rk,s		26	52	92	233	454	786	1165	157/
Partial safety factor		[IN.III] [-]	20	52	92		4 <u>54</u> 56	/00	1105	1574
	γMs		30	60	105	266	519	898	1332	1700
Stainless steel grade <b>A4-80</b> Partial safety factor	M <sup>o</sup> Rk,s		30	60	105		33	090	1332	1795
Stainless steel grade <b>1.4529</b>	γ <sub>Ms</sub> M <sup>o</sup> Rk,s		26	52	92	233	454	786	1165	157/
Partial safety factor		[IN.III] [-]	20	52	92		4 <u>54</u> 25	/00	1105	1574
Stainless steel grade <b>1.4565</b>	γMs		06	52	00	-		706	1165	157/
	M <sup>o</sup> Rk,s		26	52	92		454 56	786	1165	1574
Partial safety factor Concrete pry-out failure	γMs	[-]				١,	00			
		L T 1	1				2			
Factor for resistance to pry-out failure	$\frac{k_8}{\gamma_2^{(1)}=\gamma_{inst}^{(2)}}$						<u></u> ,0			
	/2 <sup>-</sup> /≕γinst <sup>_/</sup>	[-]				I	,0			
Concrete edge failure			M8	M10	M12	M16	M20	M24	M27	M30
Concrete edge failure Size										
	d <sub>nom</sub>	[mm]	8	10	12	16	20	24	27	30
Size		[mm] [mm]	8	10			20 , 8 d <sub>nor</sub>		27	30

### MO-H, MO-HW, MO-HS steel bonded anchor

 Table C3:
 Design method EN 1992-4

#### Performances

Design according to EN 1992-4 Characteristic resistance for shear loads - threaded rod

# Table C4: Design method EN 1992-4 Characteristic values of resistance to shear load of rebar

Steel failure without lever arm											
Size			Ø8	Ø10	Ø12	Ø16	Ø20	Ø25	Ø32		
Rebar BSt 500 S	$V_{Rk,s}$	[kN]	14	22	31	55	86	135	221		
Partial safety factor	γMs	[-]				1,5					
Characteristic resistance of group	of fasteners										
Ductility factor $k_7 = 1,0$ for steel w	ith rupture elon	gation	$A_5 > 8$	%							

Steel failure with lever arm									
Size			Ø8	Ø10	Ø12	Ø16	Ø20	Ø25	Ø32
Rebar BSt 500 S	$M^{o}_{Rk,s}$	[N.m]	33	65	112	265	518	1013	2122
Partial safety factor	γMs	[-]				1,5			
Concrete pry-out failure									
Factor for resistance to pry-out failure	e k <sub>8</sub>	[-]				2			
Installation safety factor	$\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[-]				1,0			

Concrete edge failure									
Size			Ø8	Ø10	Ø12	Ø16	Ø20	Ø25	Ø32
Outside diameter of fastener	dnom	[mm]	8	10	12	16	20	25	32
Effective length of fastener	<b>l</b> f	[mm]			min	(h <sub>ef</sub> , 8 d	J <sub>nom</sub> )		
Installation safety factor	fety factor $\gamma_2^{1} = \gamma_{inst}^{2}$ [-] 1,0								

<sup>1)</sup> Design according EOTA Technical Report TR 055

<sup>2)</sup> Design according EN 1992-4:2016

#### MO-H, MO-HW, MO-HS steel bonded anchor

**Performances** Design according to EN 1992-4 Characteristic resistance for shear loads - rebar

Anchor size			M8	M10	M12	M16	M20	M24	M27	M30
Uncracked concrete										
Tension load	F	[kN]	6,3	7,9	11,9	15,9	23,8	29,8	37,7	45,6
Displacement	δ <sub>N0</sub>	[mm]	0,3	0,3	0,3	0,3	0,4	0,5	0,5	0,5
	$\delta_{N\infty}$	[mm]	0,5	0,5	0,5	0,5	0,5	0,5	0,5	0,5
Shear load	F	[kN]	3,1	5,0	7,2	13,5	21,0	30,3	39,4	48,0
Displacement	δνο	[mm]	1,5	1,5	1,5	1,5	2,0	2,5	2,5	2,5
	δv∞	[mm]	2,3	2,3	2,3	2,3	3,0	3,8	3,8	3,8
Cracked concrete										
Tension load	F	[kN]		5,1	7,4	13,1	20,5	24,6		
Displacement	δ <sub>N0</sub>	[mm]		0,4	0,7	0,7	0,7	0,6		

## MO-H, MO-HW, MO-HS steel bonded anchor

#### Performances

Displacement for threaded rod

Table C6: Displacement of rebar under tension and shear load											
Rebar size			Ø8	Ø10	Ø12	Ø16	Ø20	Ø25	Ø32		
Uncracked concrete											
Tension load	F	[kN]	7,9	9,9	13,9	23,8	29,8	55,6	55,6		
Displacement	δ <sub>N0</sub>	[mm]	0,3	0,3	0,3	0,4	0,4	0,5	0,5		
	$\delta_{N\infty}$	[mm]	0,5	0,5	0,5	0,5	0,5	0,5	0,5		
Shear load	F	[kN]	5,9	9,3	13,3	23,7	37,0	57,9	94,8		
Displacement	δνο	[mm]	0,3	0,4	0,4	0,4	0,4	0,5	0,9		
	δv∞	[mm]	0,5	0,6	0,6	0,6	0,6	0,8	1,4		

### MO-H, MO-HW, MO-HS steel bonded anchor

## Performances

Annex C 6

Displacement for rebar

Size			M10	M12	M16	M20	M24
Tension load							
Steel failure							
Characteristic resistance grade 4.6	N <sub>Rk,s,eq</sub>	[kN]	23	34	63	98	141
Partial safety factor	γMs	[-]			2,00		
Characteristic resistance grade 5.8	$N_{Rk,s,eq}$	[kN]	29	42	79	123	177
Partial safety factor	γMs	[-]			1,50	•	
Characteristic resistance grade 8.8	N <sub>Rk,s,eq</sub>	[kN]	46	67	126	196	282
Partial safety factor	γMs	[-]			1,50		-
Characteristic resistance grade 10.9	N <sub>Rk,s,eq</sub>	[kN]	58	84	157	245	353
Partial safety factor	γMs	[-]			1,33		
Characteristic resistance A2-70, A4-70	$N_{Rk,s,eq}$	[kN]	41	59	110	172	247
Partial safety factor	γMs	[-]			1,87		
Characteristic resistance A4-80	$N_{Rk,s,eq}$	[kN]	46	67	126	196	282
Partial safety factor	γMs	[-]			1,60		
Characteristic resistance 1.4529	N <sub>Rk,s,eq</sub>	[kN]	41	59	110	172	247
Partial safety factor	γMs	[-]			1,50		
Characteristic resistance 1.4565	N <sub>Rk,s,eq</sub>	[kN]	41	59	110	172	247
Partial safety factor	γMs	[-]			1,87		
Combined pull-out and concrete cone	e failure						
Dry and wet concrete		[N/mm <sup>2</sup> ]	3,5	3,5	3,5	3,5	3,5
Installation safety factor	$\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[-]			1,2		
Flooded hole		[N/mm <sup>2</sup> ]	3,5	3,5	3,5	3,5	3,5
Installation safety factor	$\gamma_2^{(1)} = \gamma_{inst}^{(2)}$	[-]			1,4		
Shear load							
Steel failure without lever arm							
Characteristic resistance grade 4.6	$V_{Rk,s,eq}$	[kN]	7	10	23	30	40
Partial safety factor	γMs	[-]			1,67		
Characteristic resistance grade 5.8	$V_{Rk,s,eq}$	[kN]	9	13	28	38	51
Partial safety factor	γMs	[-]			1,25		
Characteristic resistance grade 8.8	$V_{Rk,s,eq}$	[kN]	14	21	45	61	81
Partial safety factor	γMs	[-]			1,25		
Characteristic resistance grade 10.9	V <sub>Rk,s,eq</sub>	[kN]	18	26	56	76	101
Partial safety factor	γMs	[-]			1,50		
Characteristic resistance A2-70, A4-70	$V_{Rk,s,eq}$	[kN]	12	18	39	53	71
Partial safety factor	γMs	[-]			1,56		
Characteristic resistance A4-80	V <sub>Rk,s,eq</sub>	[kN]	14	21	45	61	81
Partial safety factor	γMs	[-]			1,33		-
Characteristic resistance 1.4529	$V_{Rk,s,eq}$	[kN]	12	18	39	53	71
Partial safety factor	γMs	[-]			1,25		
Characteristic resistance 1.4565	V <sub>Rk,s,eq</sub>	[kN]	12	18	39	53	71
Partial safety factor	γMs	[-]			1,56		
Factor for annular gap	$lpha_{\sf gap}$	[-]			0,5		

Table C7: Characteristic values of resistance under seismic action category C1 for threaded rods

<sup>1)</sup> Design according EOTA Technical Report TR 055
 <sup>2)</sup> Design according EN 1992-4:2016

Note: Rebars are not qualified for seismic design

#### MO-H, MO-HW, MO-HS steel bonded anchor

#### Performances

Reduction factors for seismic design